

The Dynamic Compaction of Sand and Related Porous Systems Quasi-static to Shock

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Research supported by -
AFOSR / EglinAFB/ NSWC / EOARD
QinetiQ / dstl / DTRA/ MoD (UK)

Aims

- Apply techniques to determine the high-pressure and low-pressure response of sand
- Use a natural sand (marine)
- Present data on sand over a wide range of strain rates.
- Establish trends
- Provide data for validation of models
- Increase predictive capability

Modelling

Several groups of models exist -

P-alpha model (volume-based)

P-lambda model (length-based)

Porter-Gould (potential-based)

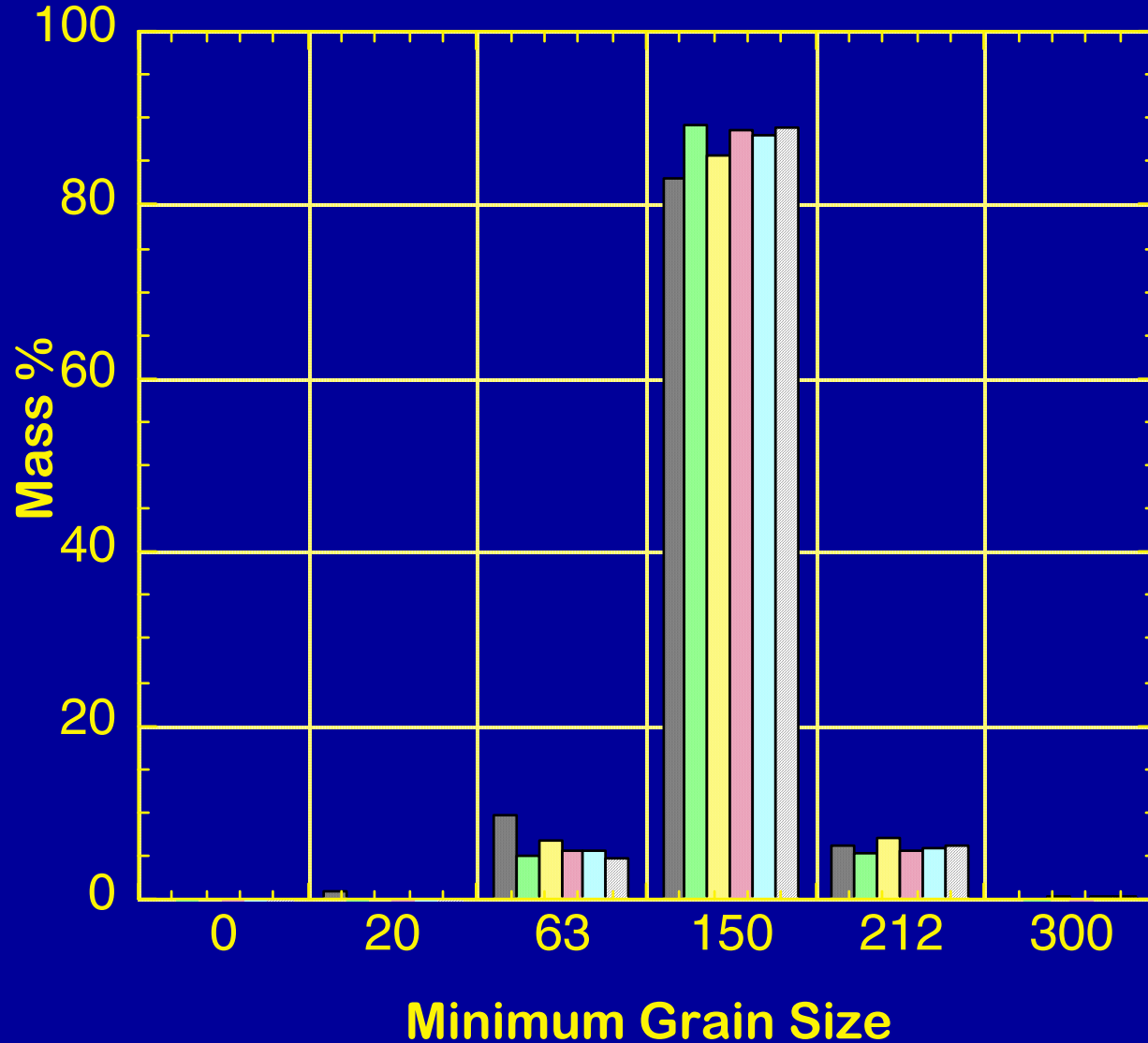
Thouvenin (laminar-based)

Parameters / Techniques

- **Dry Sand - heated in oven.**
- **5%, 10%, 20%, 22% by mass water,**
- **Instron**
- **Dropweight**
- **Hopkinson Bar**
- **Plate Impact**

Size Distribution (natural sand)

Grain Size Distribution



Sand - bi-modal mix

- Bimodal sand - 150-210 micron + 50-63 micron particles
- No significant difference found with the natural "mix".
- Both materials will be referred to as "sand"

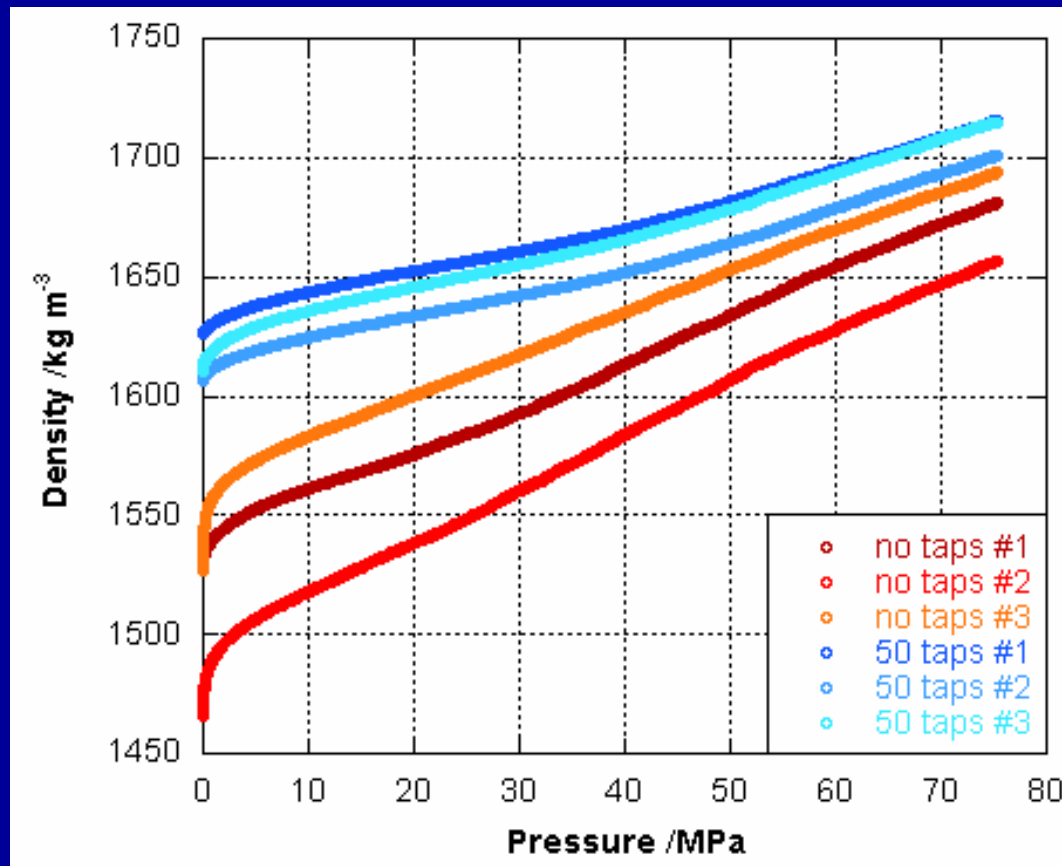
Instron - Quasi-Static



Parameter Space

- 10 kN load capacity
- Water content 0, 5 or 10 %mass.
- 6 g samples
- Stainless steel cell
 - 13 mm inner diameter
- Piston driven in at 5 mm/min.

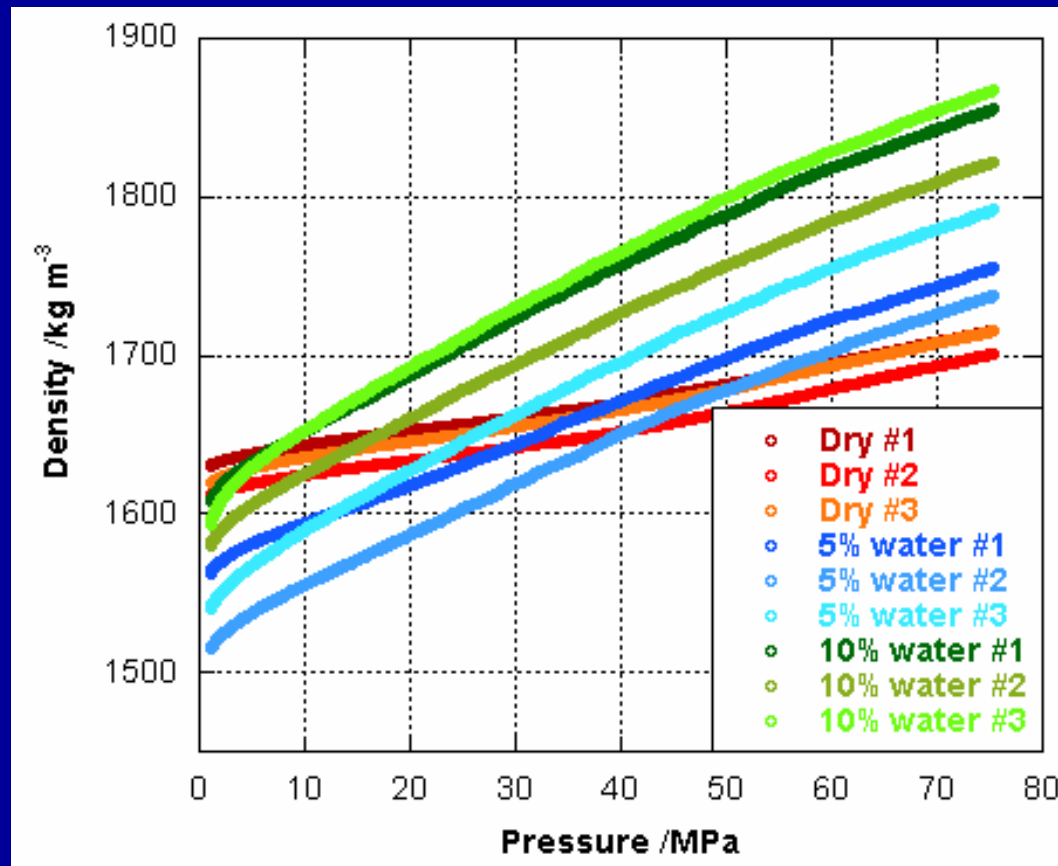
Instron - Results



Starting Density

- Obviously important
- In range the materials move closer together
- Do not become identical
- Friction between the grains
- Lock-up with pressure
- Movement of particles
- Force Chains within the sample
- Skeletal Strength

Moisture Content



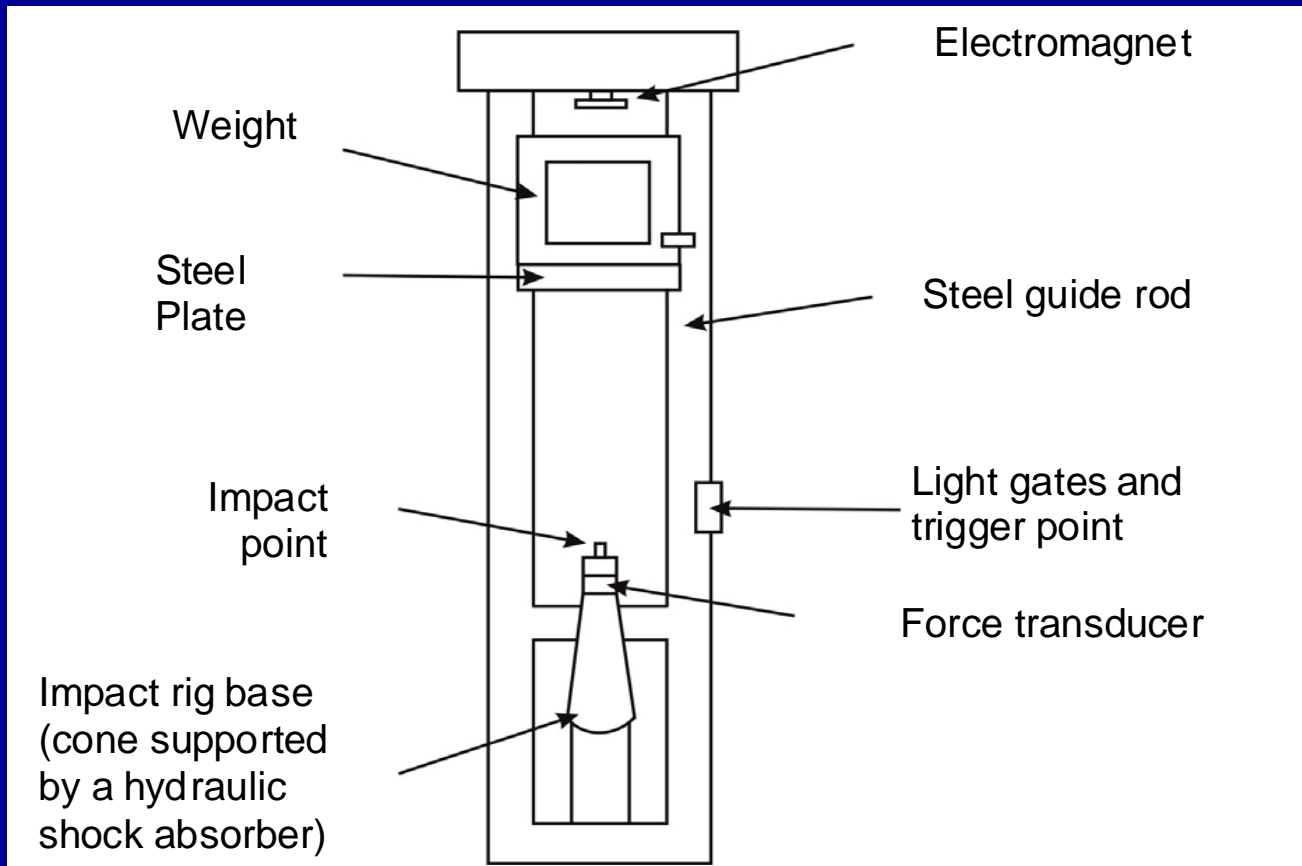
Water Content

- Starting density order
 - Dry > 10% Wet > 5% Wet
- Dry = limited change in density
- Wet = movement in grains
- Wet = move along parallel paths

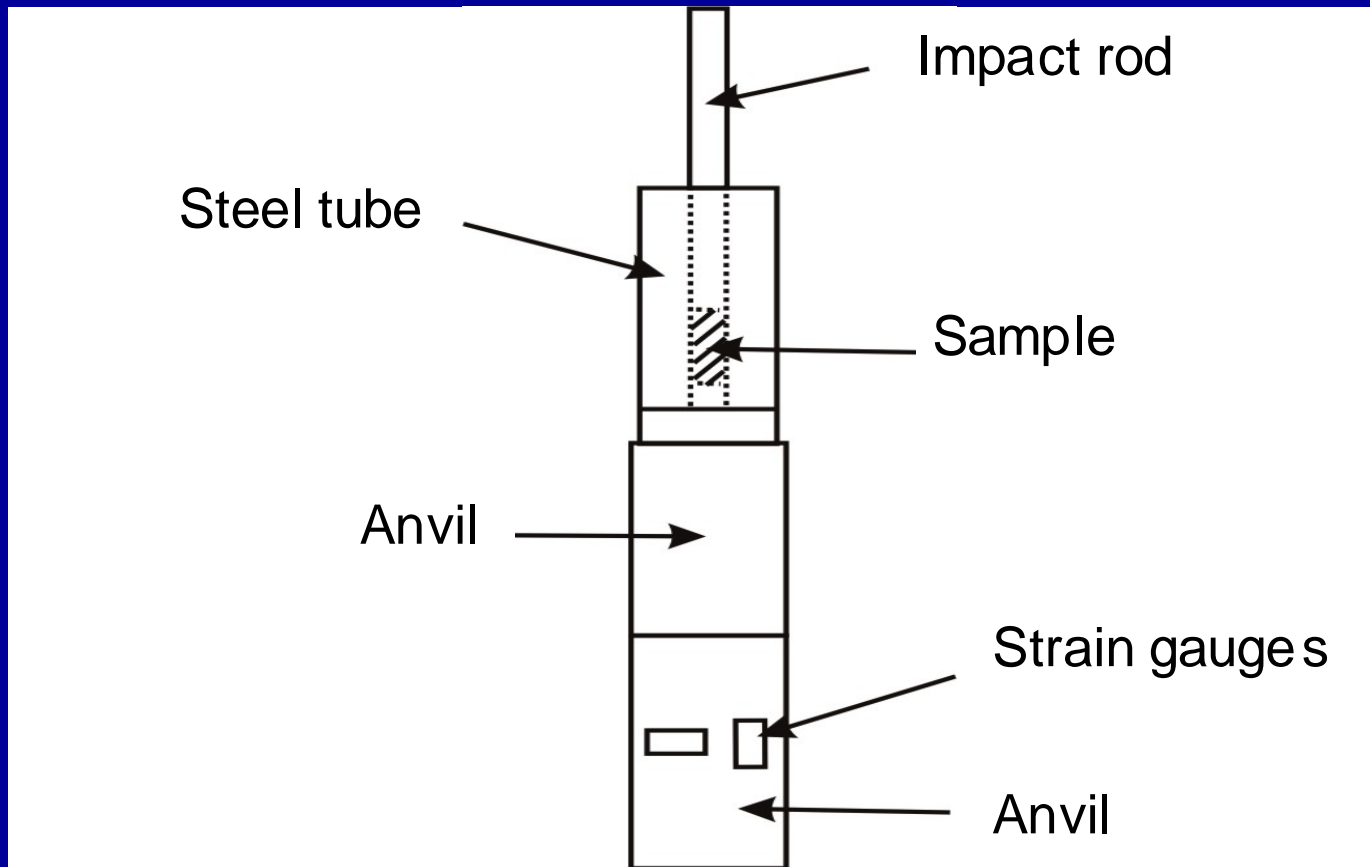
Drop-weight Parameters

- 4 orders strain-rate faster than Instron
- 6.414 kg weight
- Maximum height of 120 cm.
- Guided
- Velocities of up to 5 ms^{-1}
- Sample cell and size - same as Instron

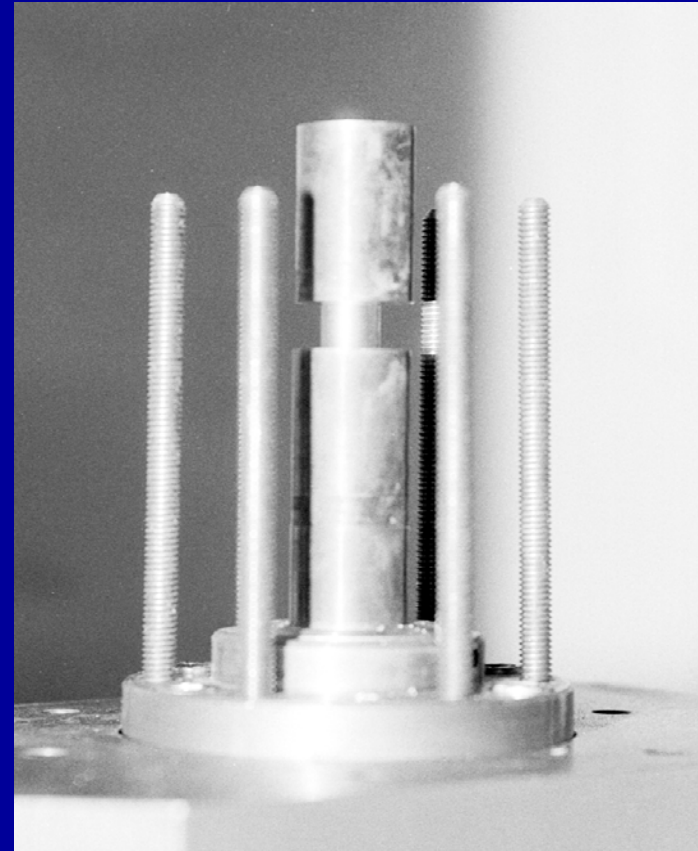
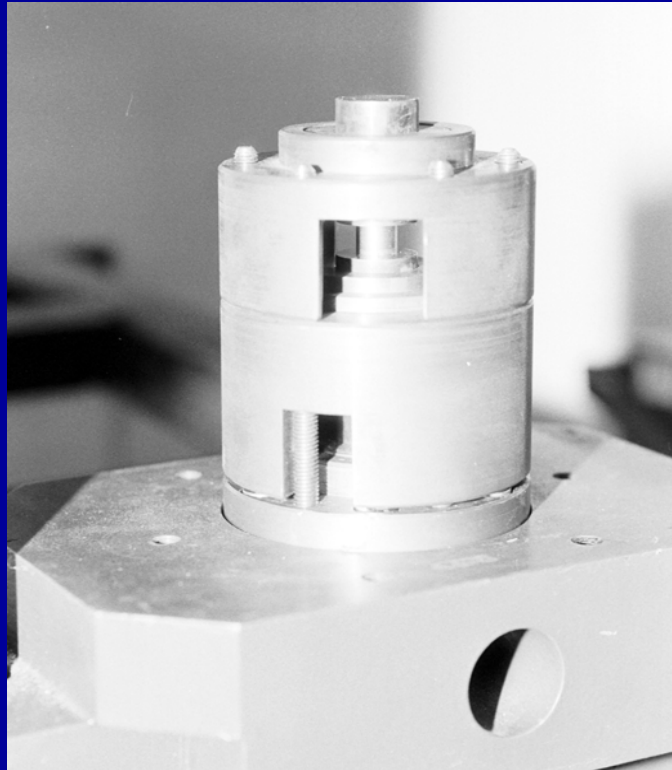
Schematic Drop-weight



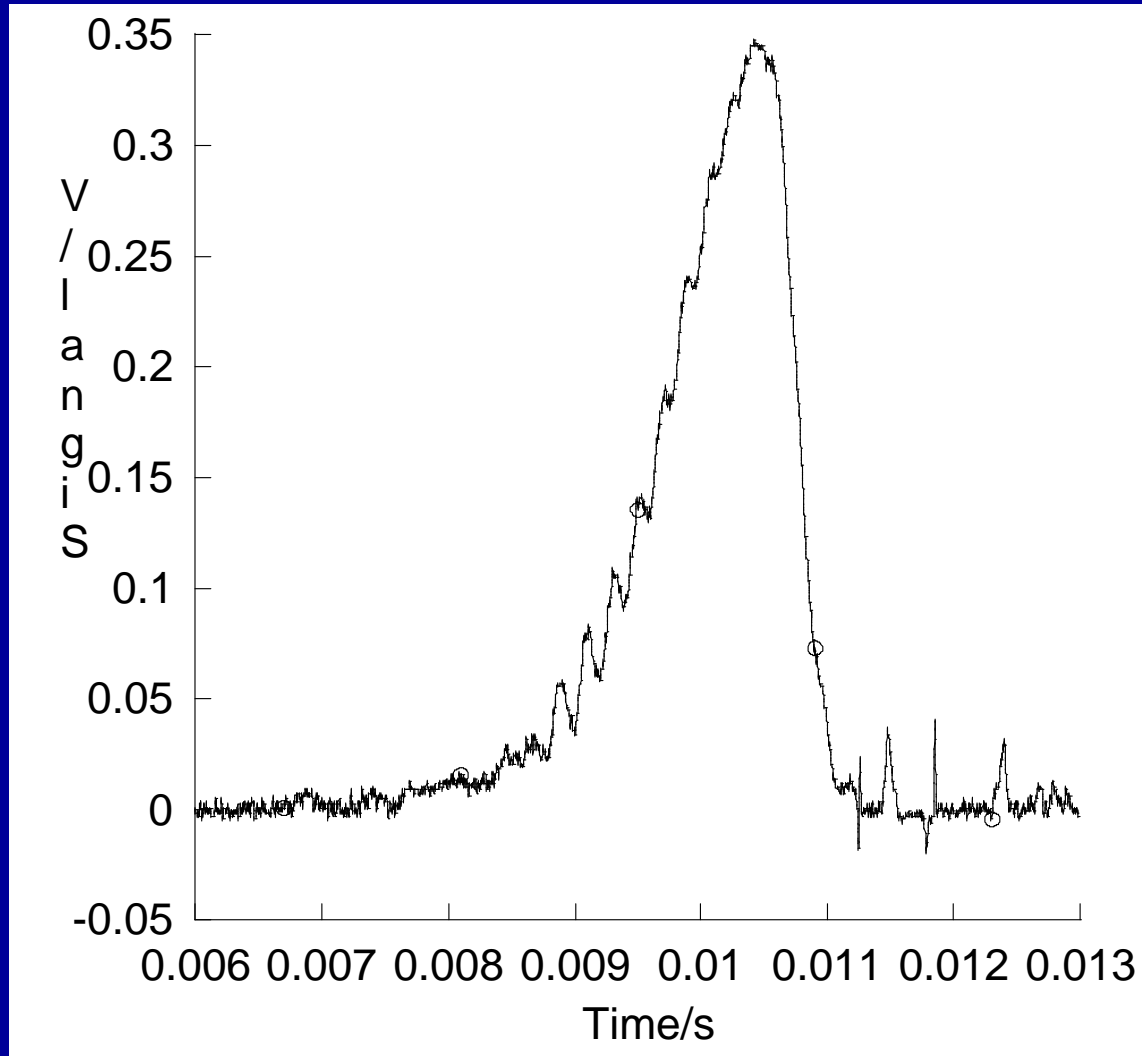
Sample Cell - Stress monitoring



Force transducer

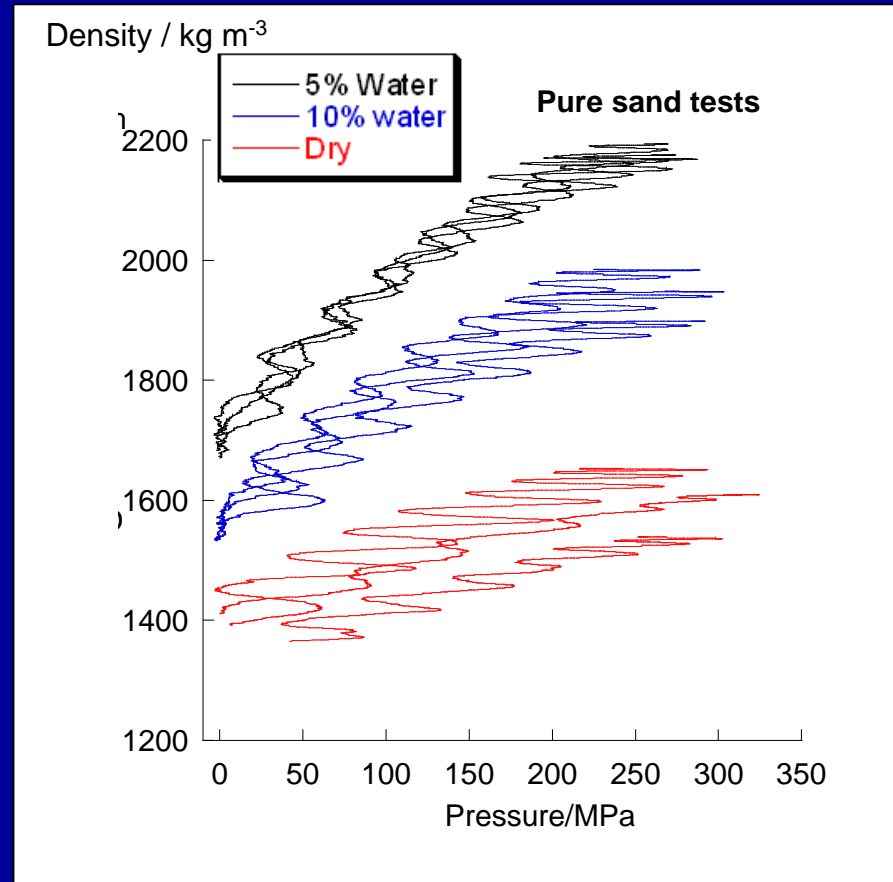


Raw Strain Signal



Stress + Deceleration (distance)

... and the results

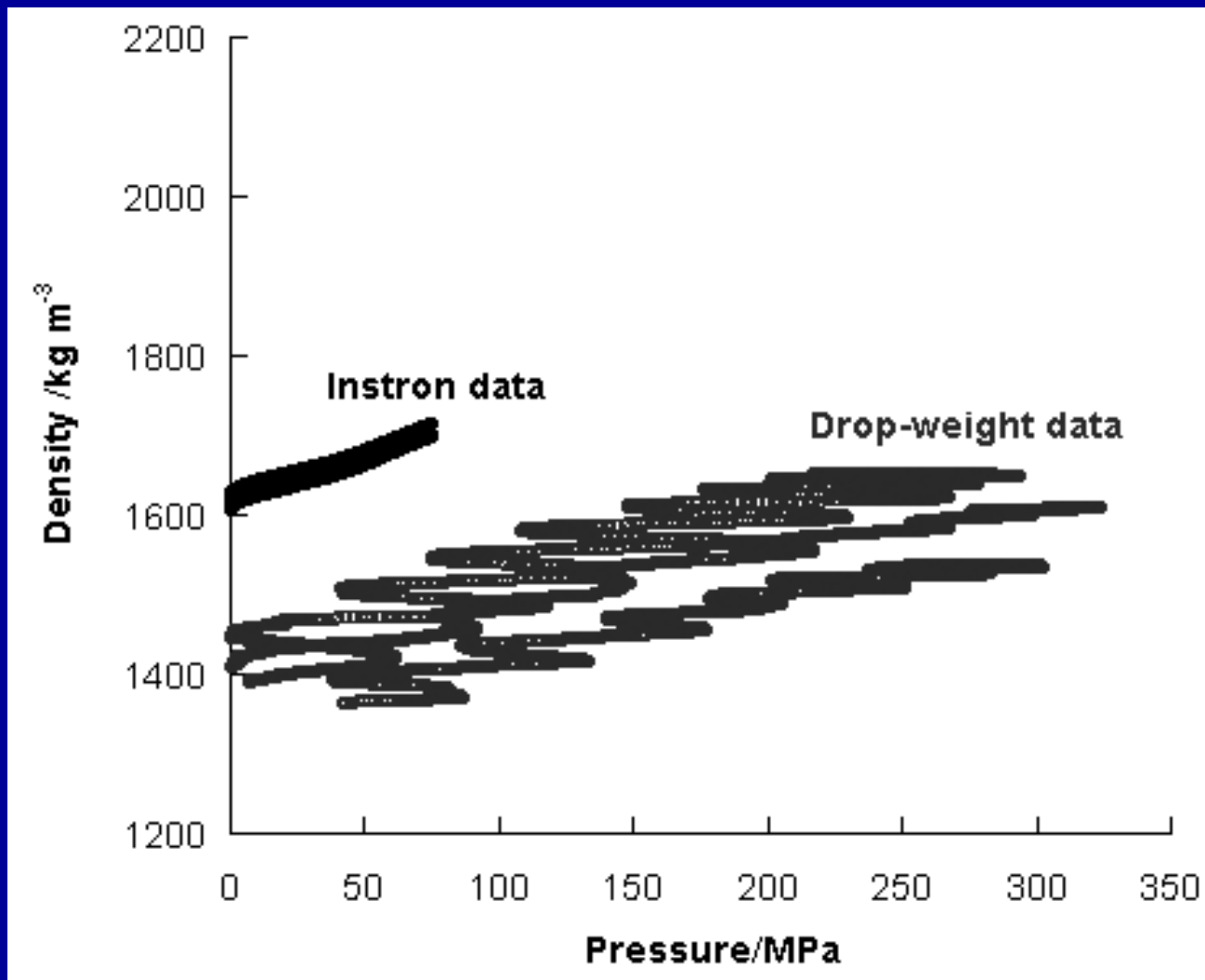


Trends

- Trends
 - Dry sand - little compaction
 - Wet sand - grain movement
 - Lubrication
 - In all cases limited fracture
- In Wet samples - see some water flow out of pores

Comparison -

Comparison - Quasi to Dropweight

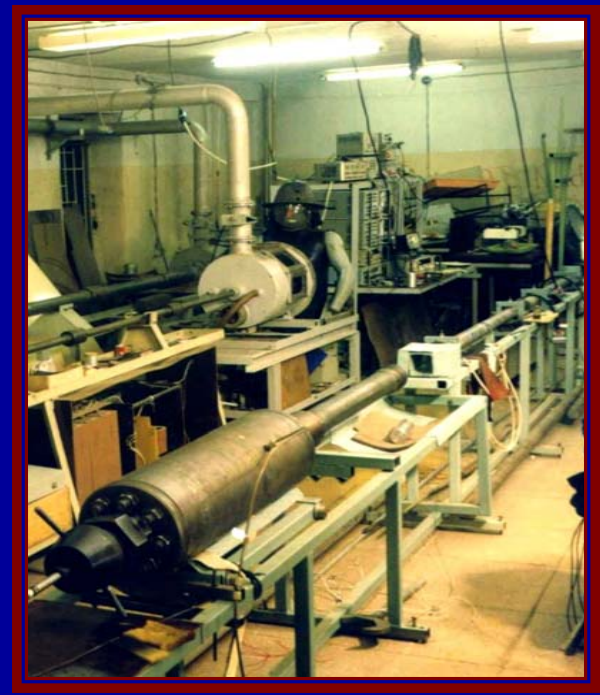
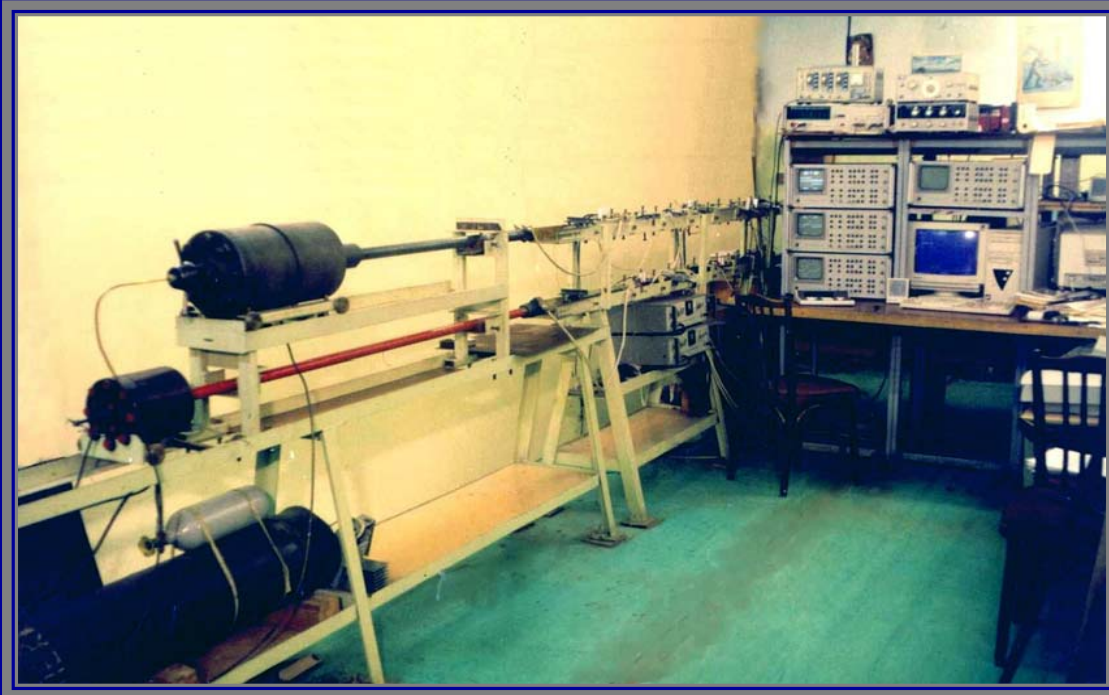


Intermediate Rates

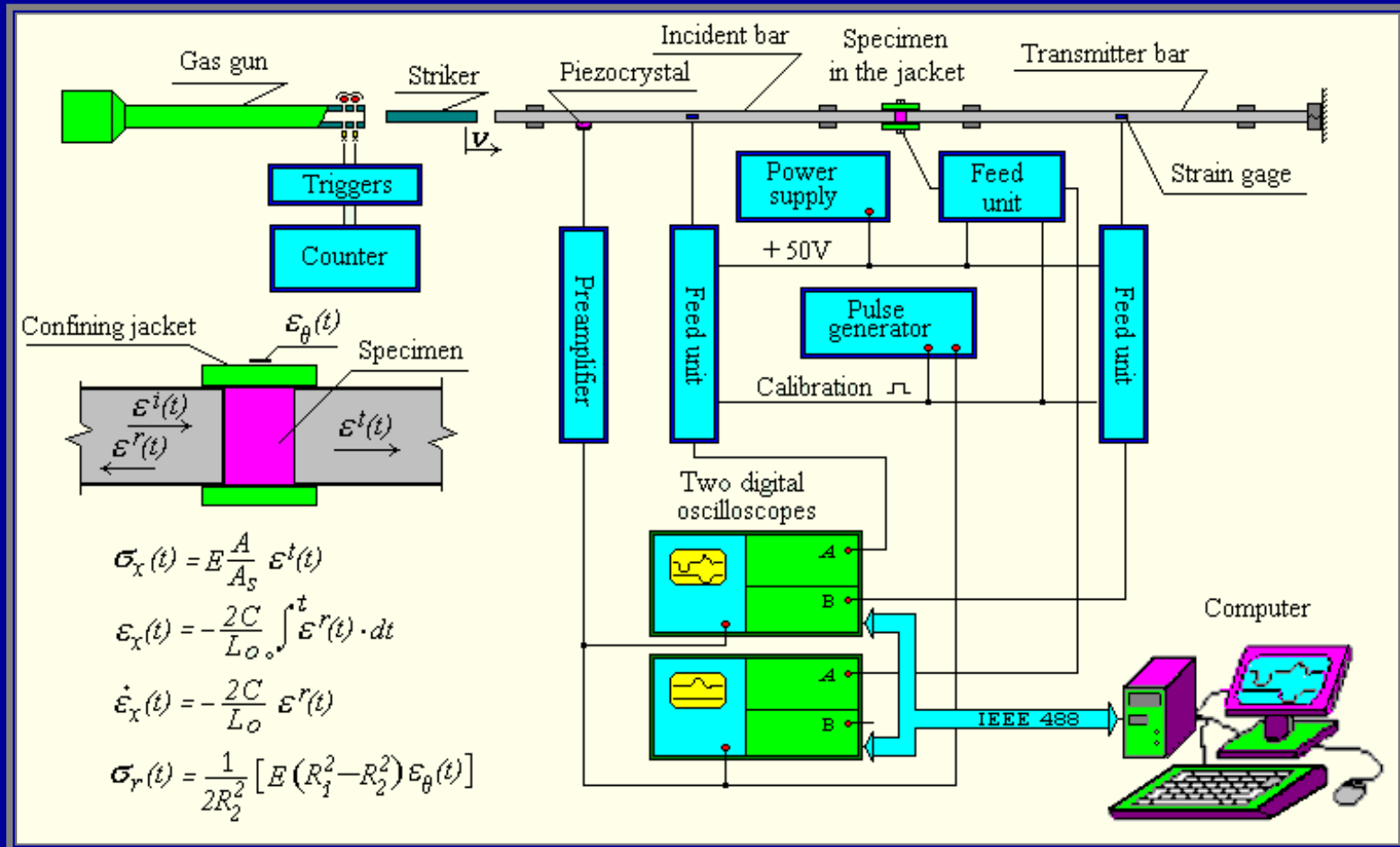
Hopkinson Bar

- Strain rate up to 10^4 s^{-1}
- Kolsky / Hopkinson Bar technique
- Bars - elastic waveguides
- Strain gauges on bars
- Stress-time / strain - time

*Set Hopkinson pressure bars
Diameter of 10/20 /60mm*

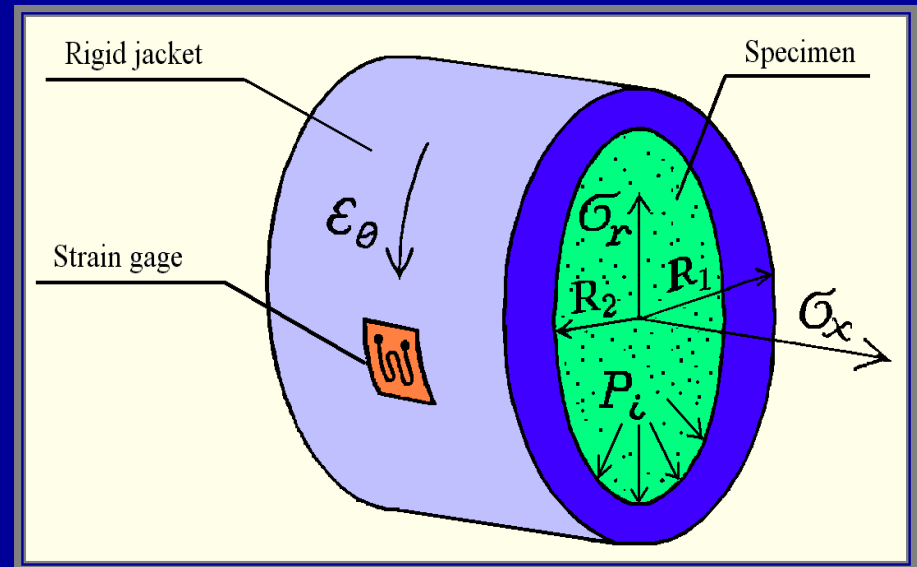


Modified Kolsky method for poorly coherent and low-density materials

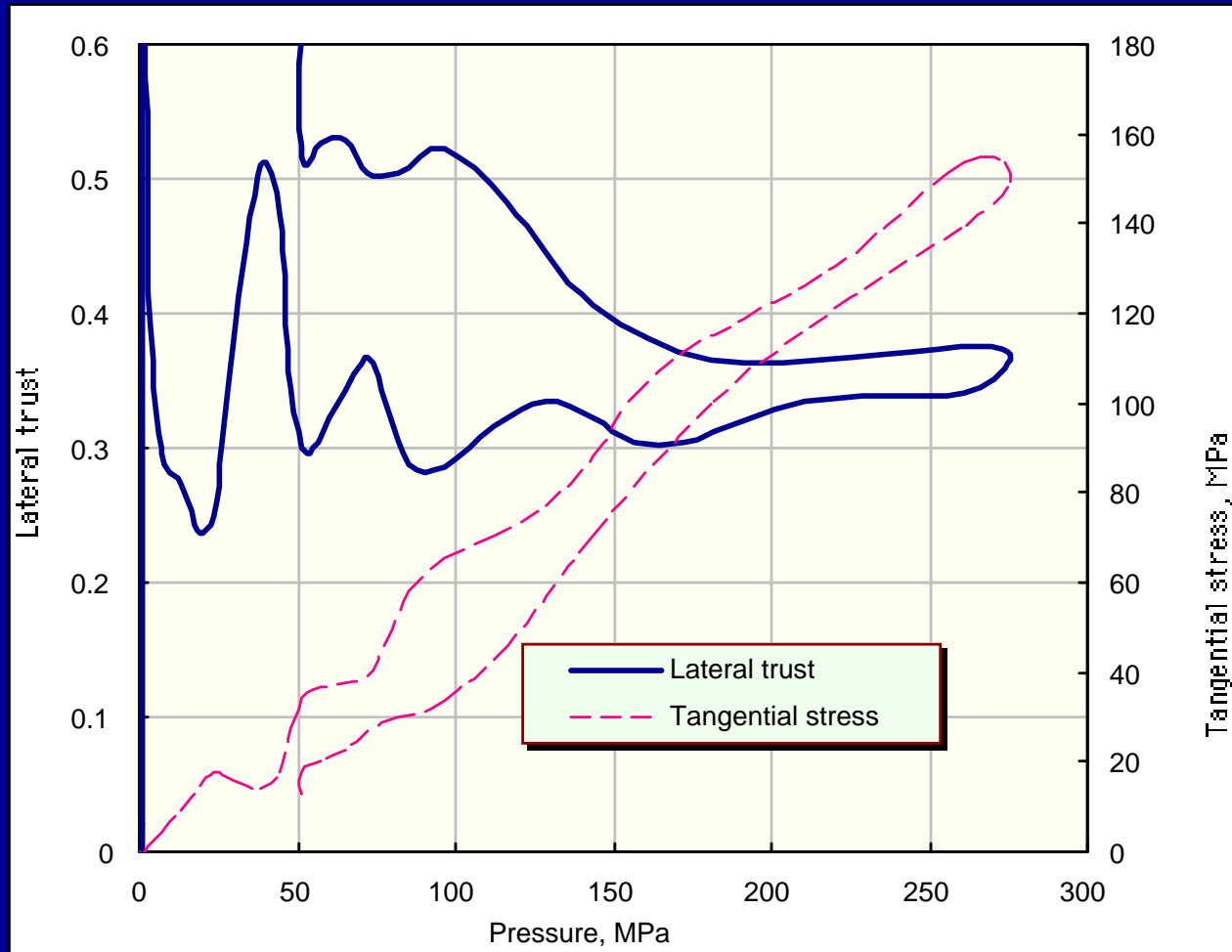


Stress / Strains in the System

**Stress components
in a specimen and in
the confined jacket**



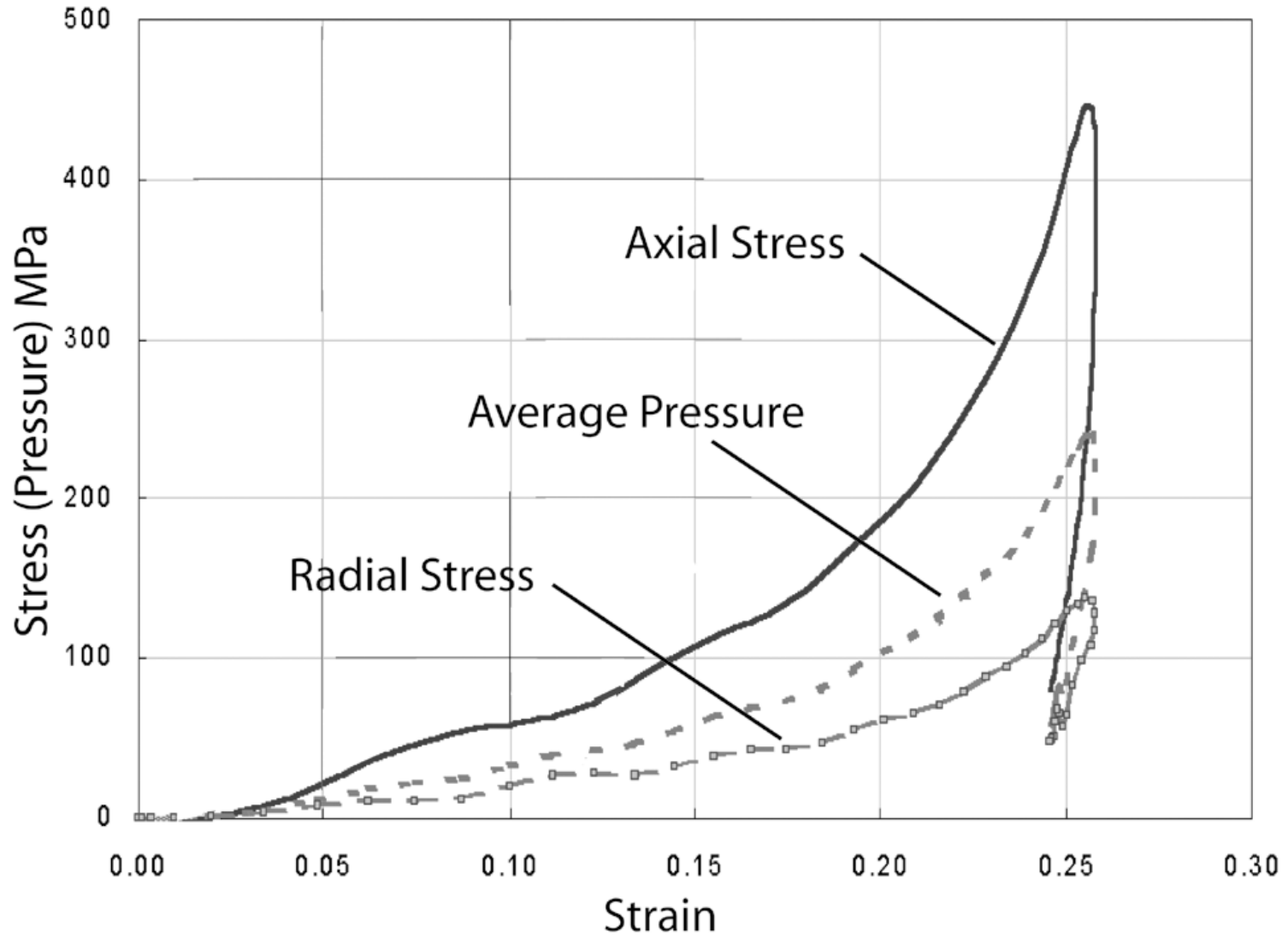
Data from Jacketed Hopkinson System



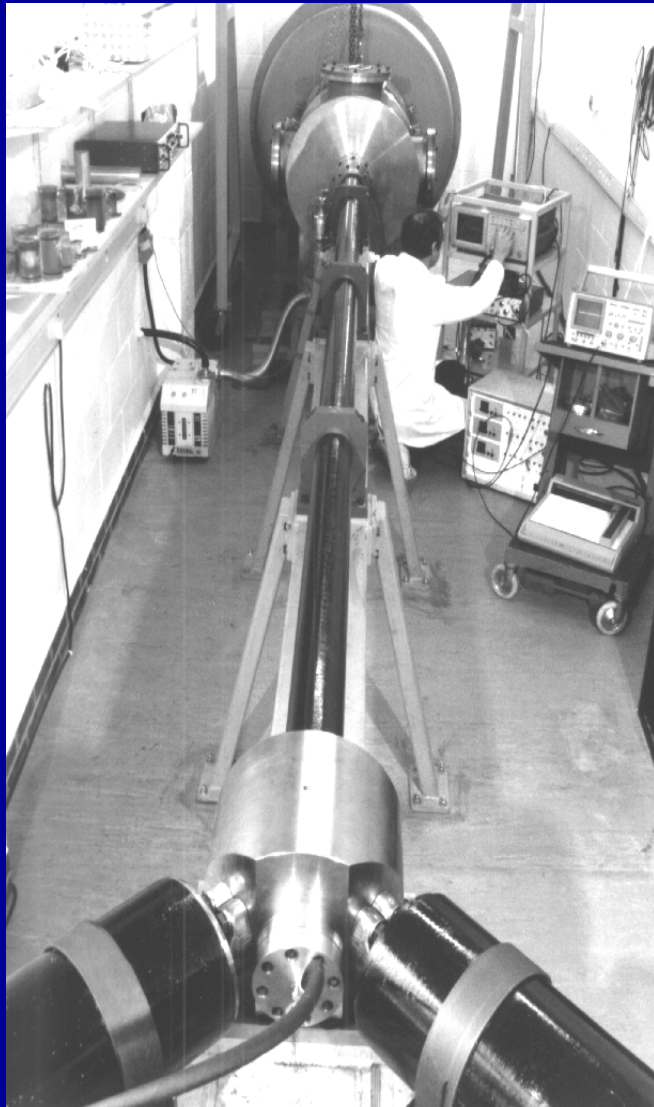
The Governing Relationships

- $\tau = (\sigma_x - \sigma_r) / 2$
- $P = (\sigma_x + 2\sigma_r) / 3$
- $\tau = C + (\tan\psi)P$
- $P = (\sigma_x - \frac{4}{3}C) / (1 + \frac{4}{3}\tan\psi)$
- Loose soils - C is small - little static shear strength

Data obtained



The Cavendish Gas-Gun Facility



*50 mm bore / 5 m long barrel
20 l gas reservoirs
350 atm. max. driving pressure
150 - 600 g projectiles
Velocities up to 1.2 km s⁻¹*



Manganin Foil Stress Gauges

Gauges - piezoresistive

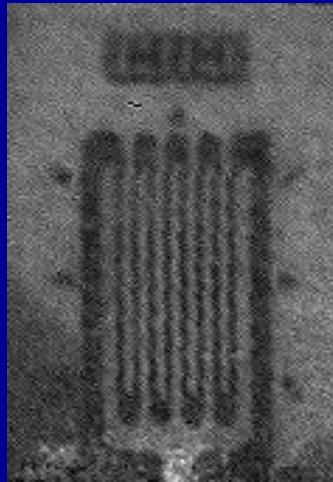
Time resolution 30 - 200 ns dependant on geometry

Accuracy $\pm 2.5\%$

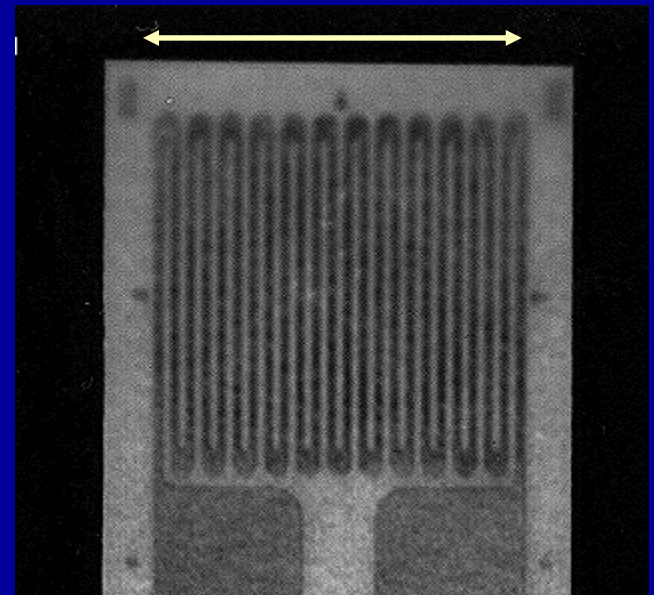
Different sizes available

Encapsulated Gauge

2.3 mm

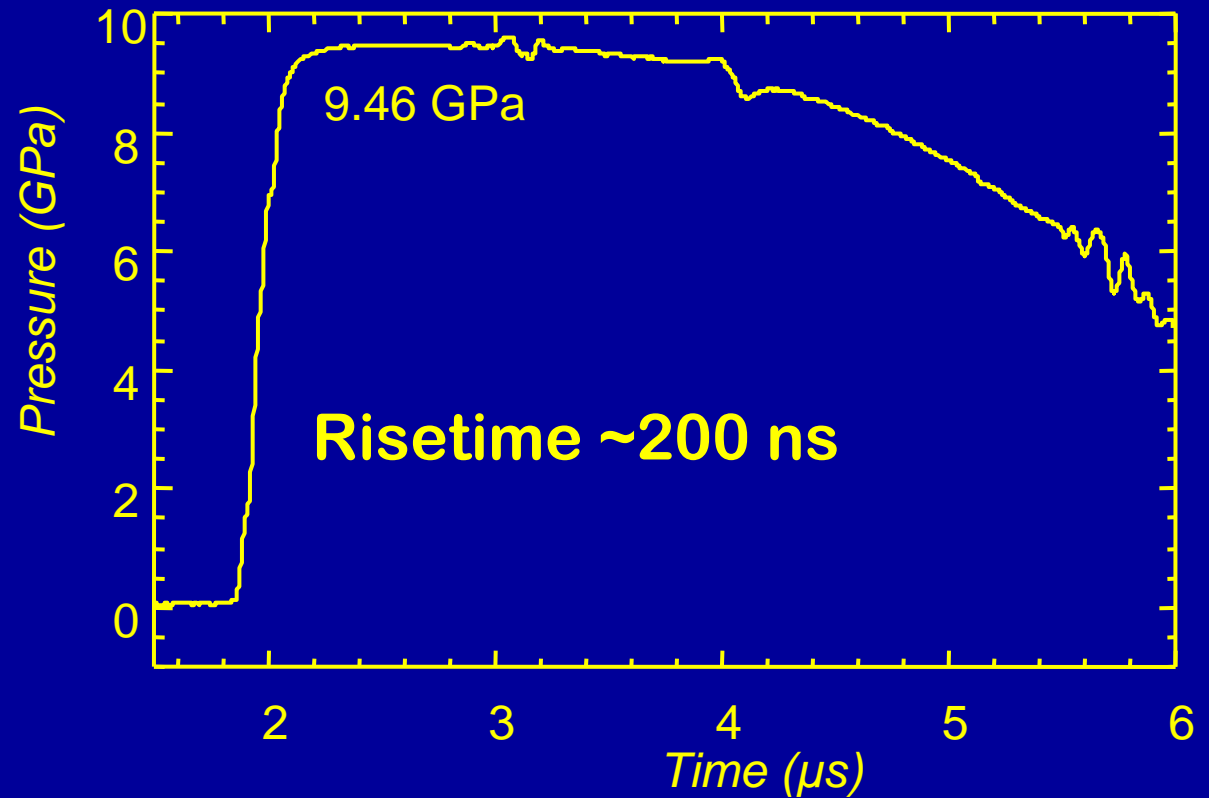
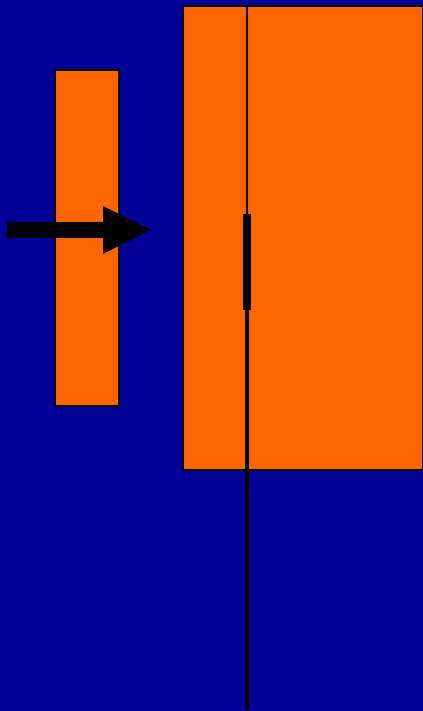


6.0 mm

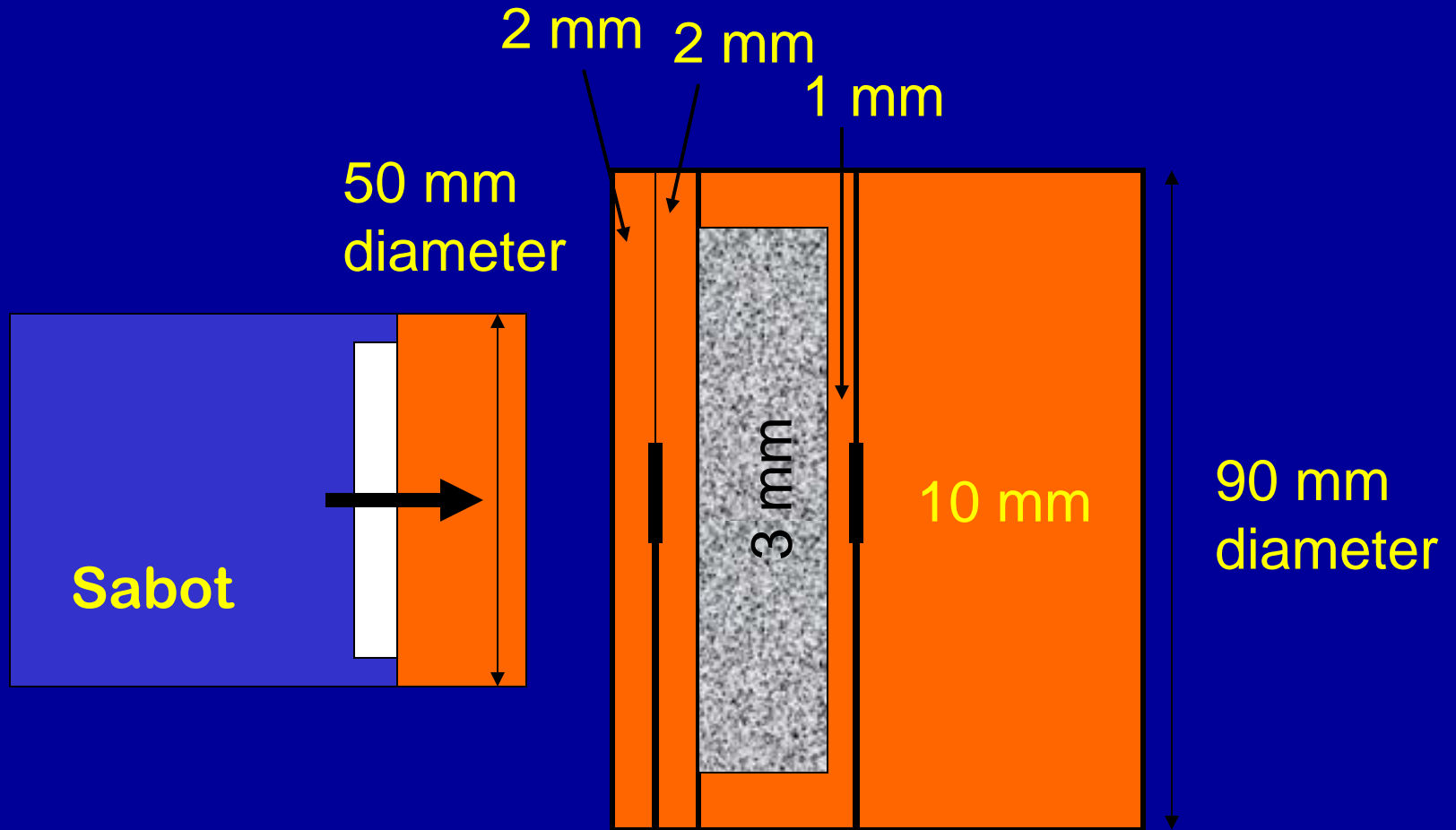


Copper Impactor on Copper Target

- Impact Velocity = 498 m s^{-1} , 10 mm Cu Flier
- Target = Impact Face / 10 mm Cu / Gauge / 20 mm Cu

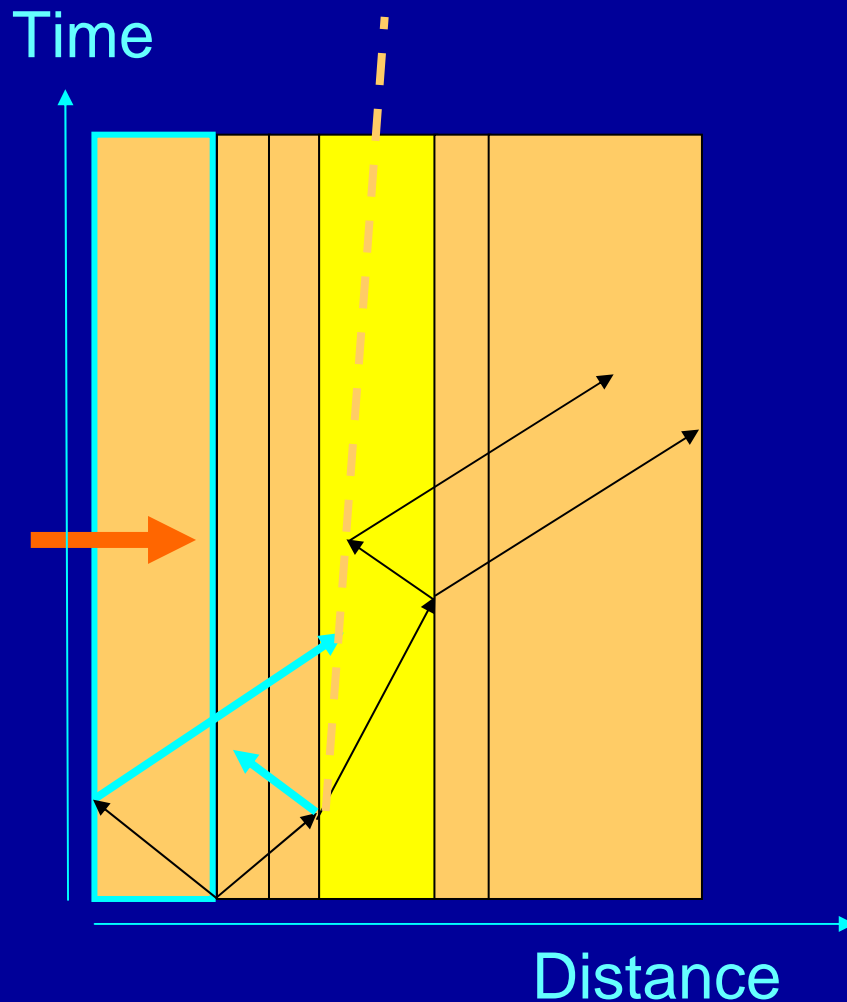


Sample Arrangement



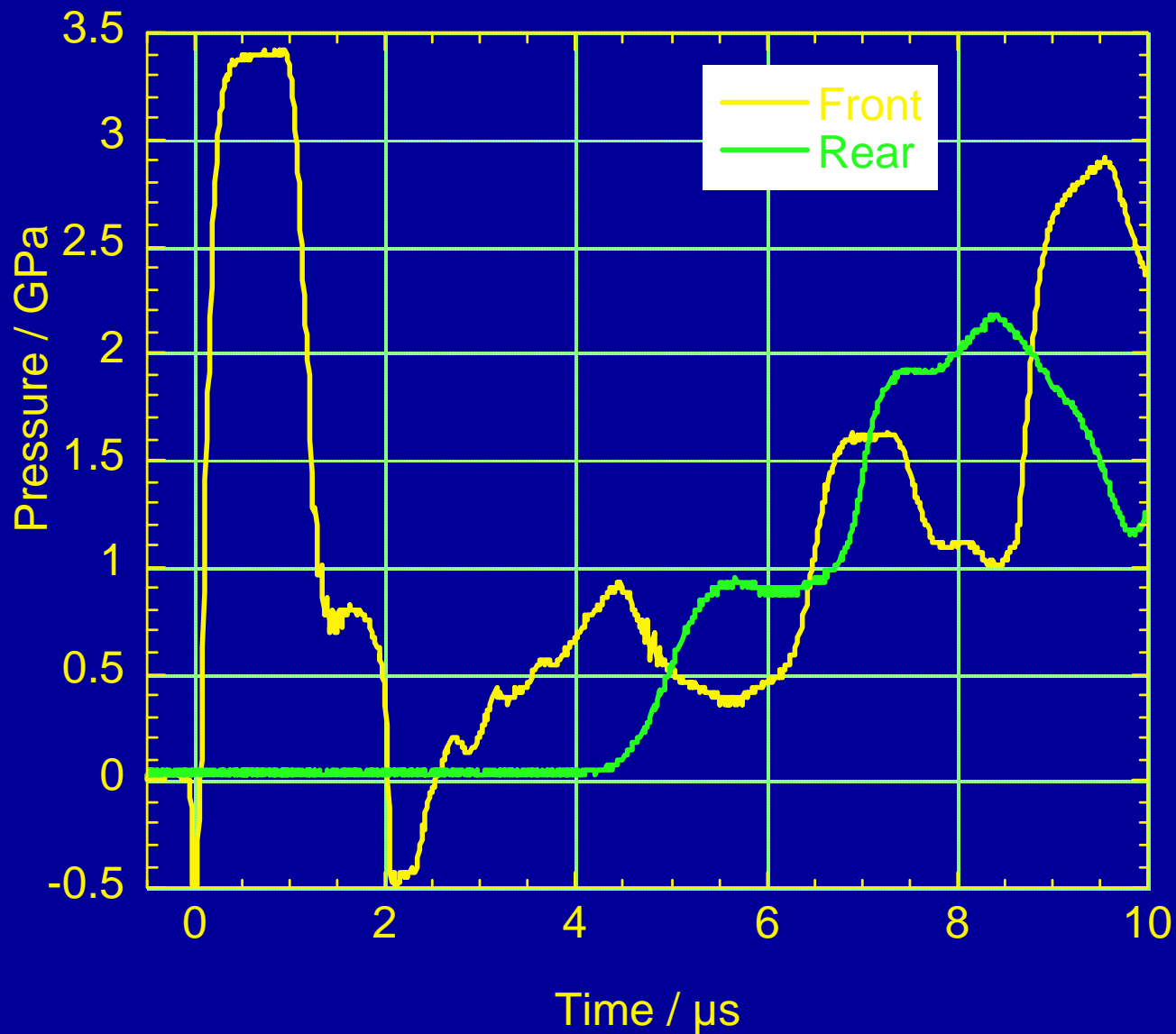
Drawing not to scale

Wave reflection in cell

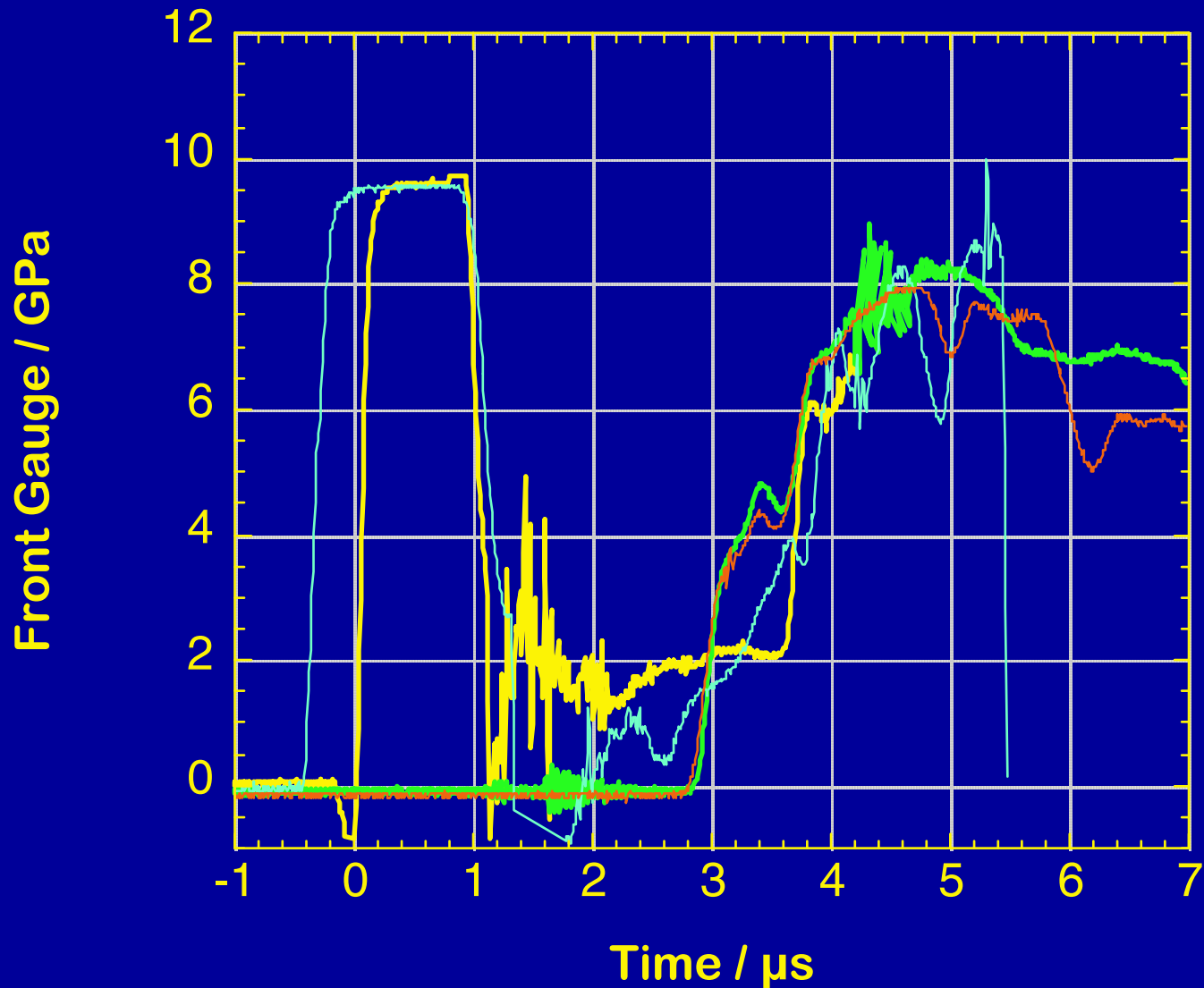


- Shock waves - black lines
- Release waves - blue lines
- Dashed line - indicates compaction

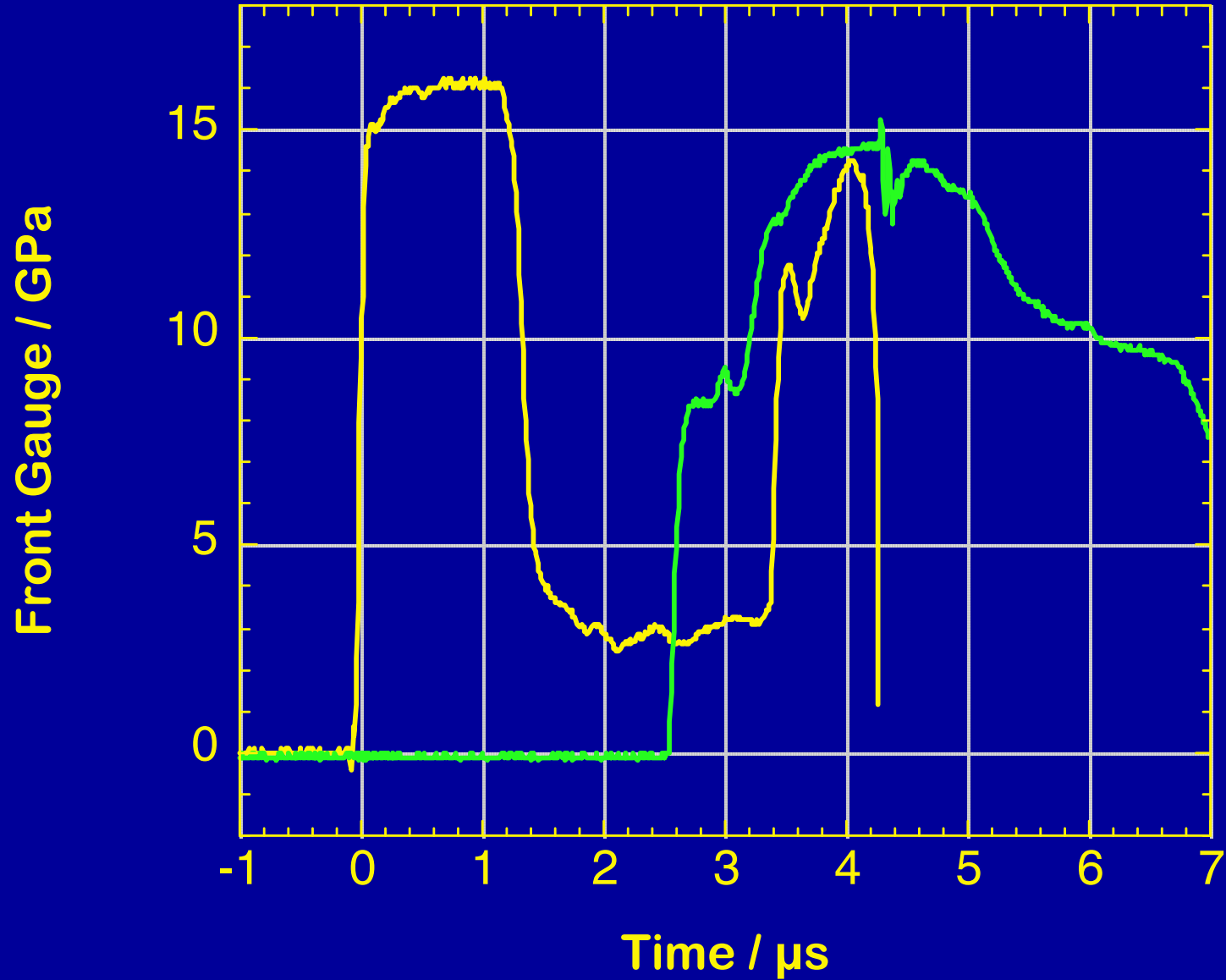
Impact at 200 m s⁻¹



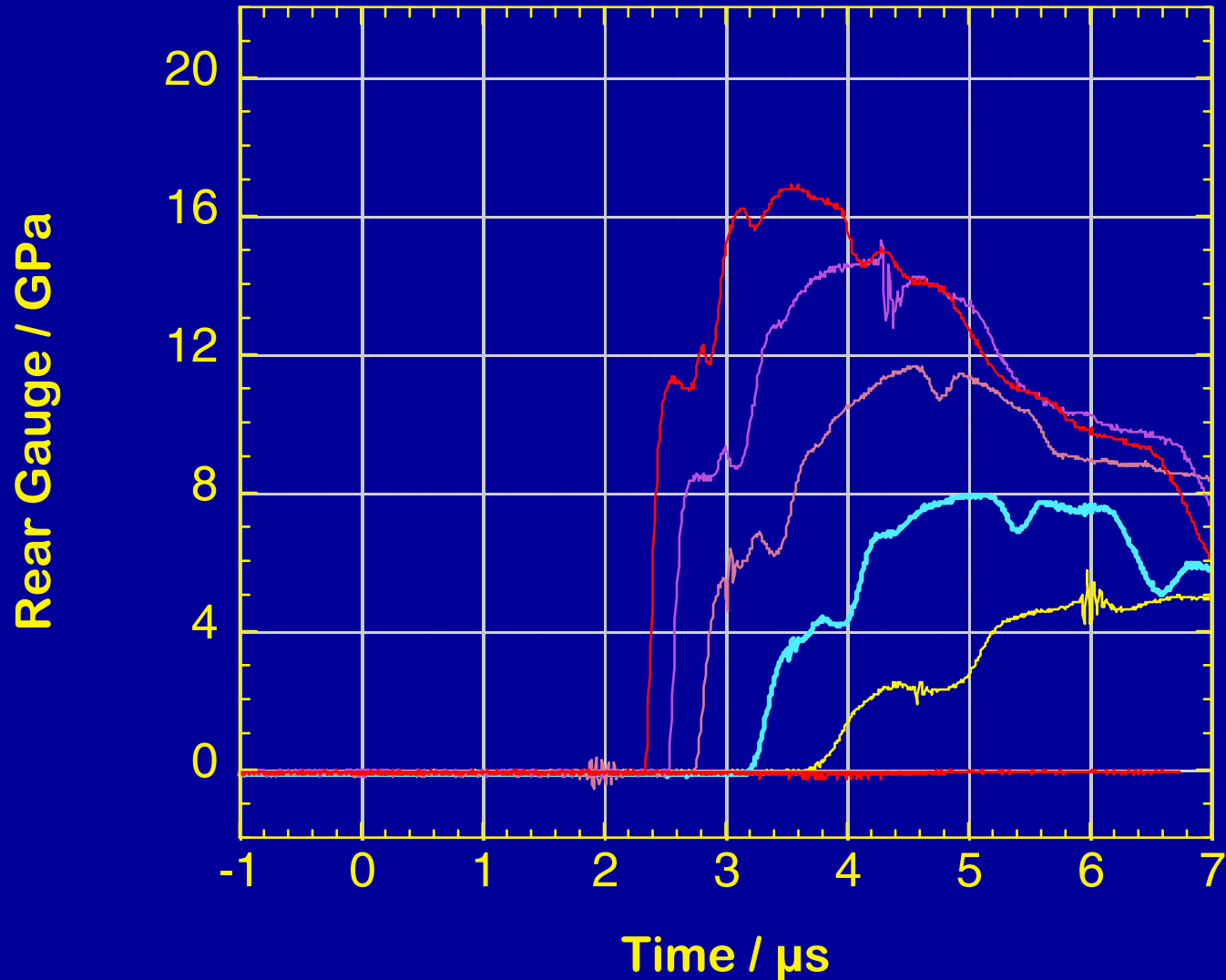
500 + 505 m s⁻¹



812 m s⁻¹



Rear Gauge Variation



Features in Output Traces

- Ramping region - pore collapse
- Shock velocity on principal Hugoniot
time difference between gauges
- 1st Plateau - secondary Hugoniot
- 2nd Plateau - ring-up, wave reflection
- Shock velocity in pre-compressed sand
(gauge comparison)

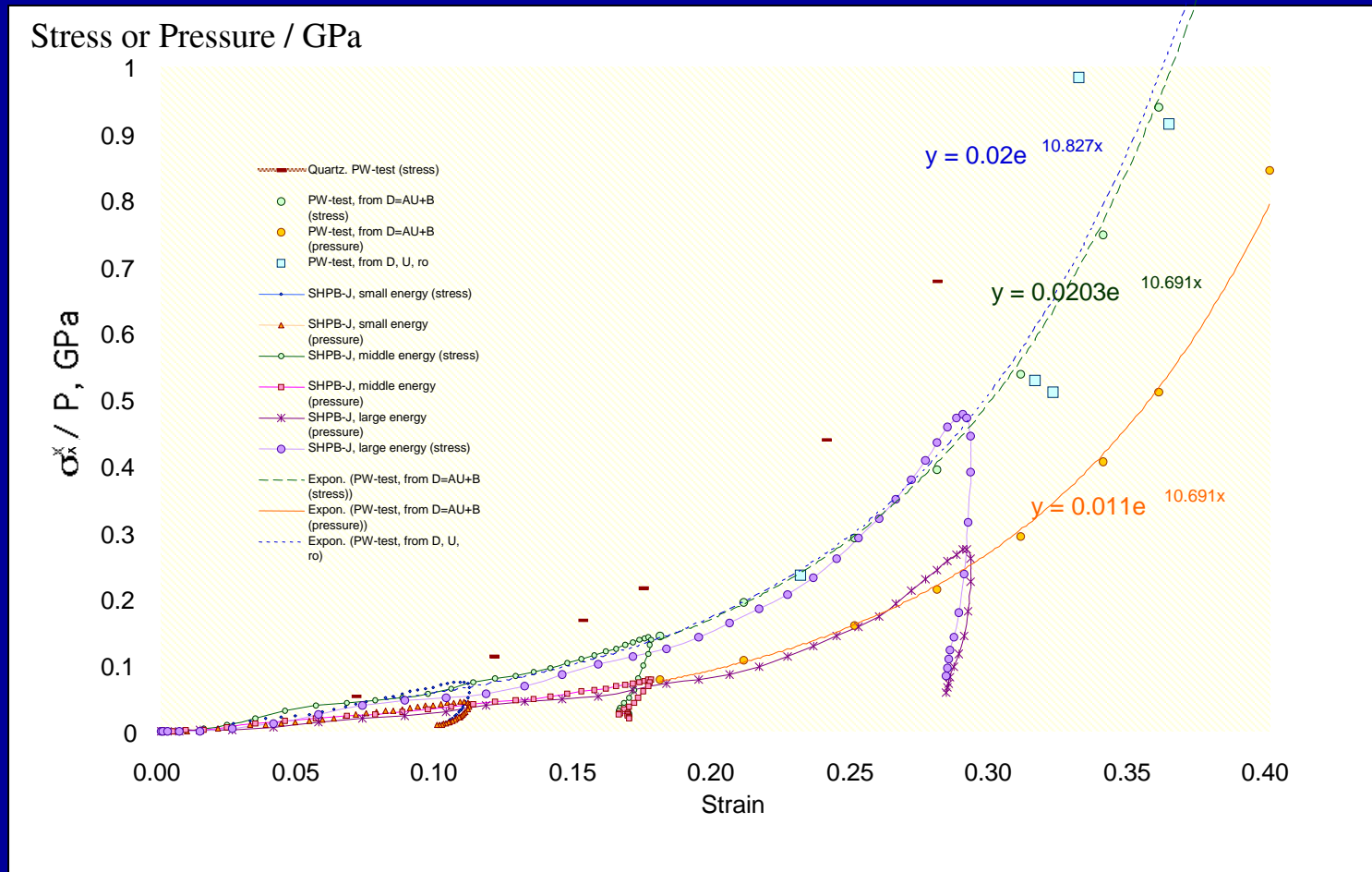
Shock thickness / particle size

- Rise time of first pulse
- Shock velocity
- 200 m s⁻¹
 - 1 μs rise time and U_s 1 mm μs⁻¹
 - 1 mm or 4 grain particles
- 500 m s⁻¹
 - 0.5 μs rise time U_s 1.4 mm μs⁻¹
 - 0.7 mm or 3 grain particles
- 800 m s⁻¹
 - 0.2 μs rise time and U_s 2 mm μs⁻¹
 - 0.4 mm or 2 grain particles
- Need appropriate length-scale model (mesoscopic)

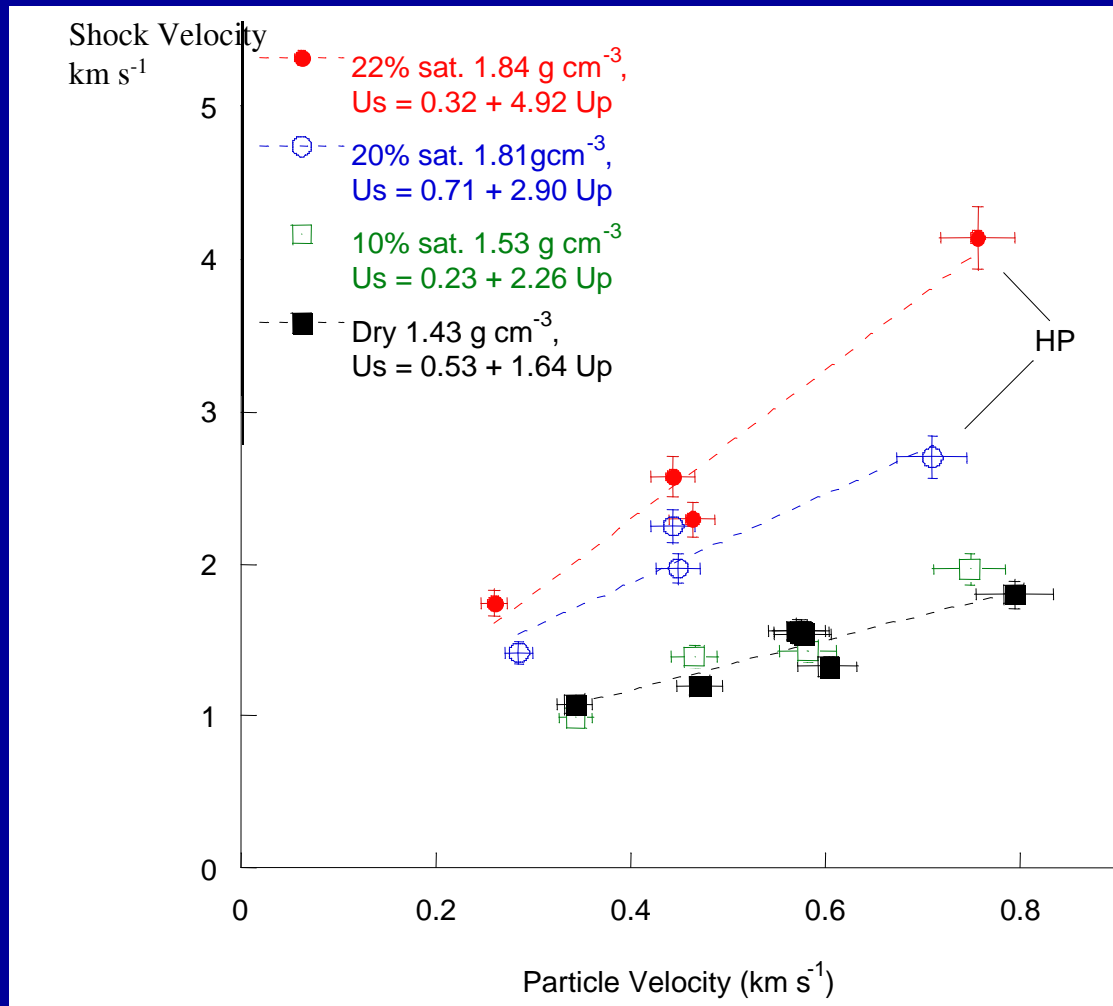
Comparison - Intermediate to High-rate

- Assume relationship lateral v. longitudinal stress ~same in shock
- Overlap of stress range of Hopkinson bar with the shock study

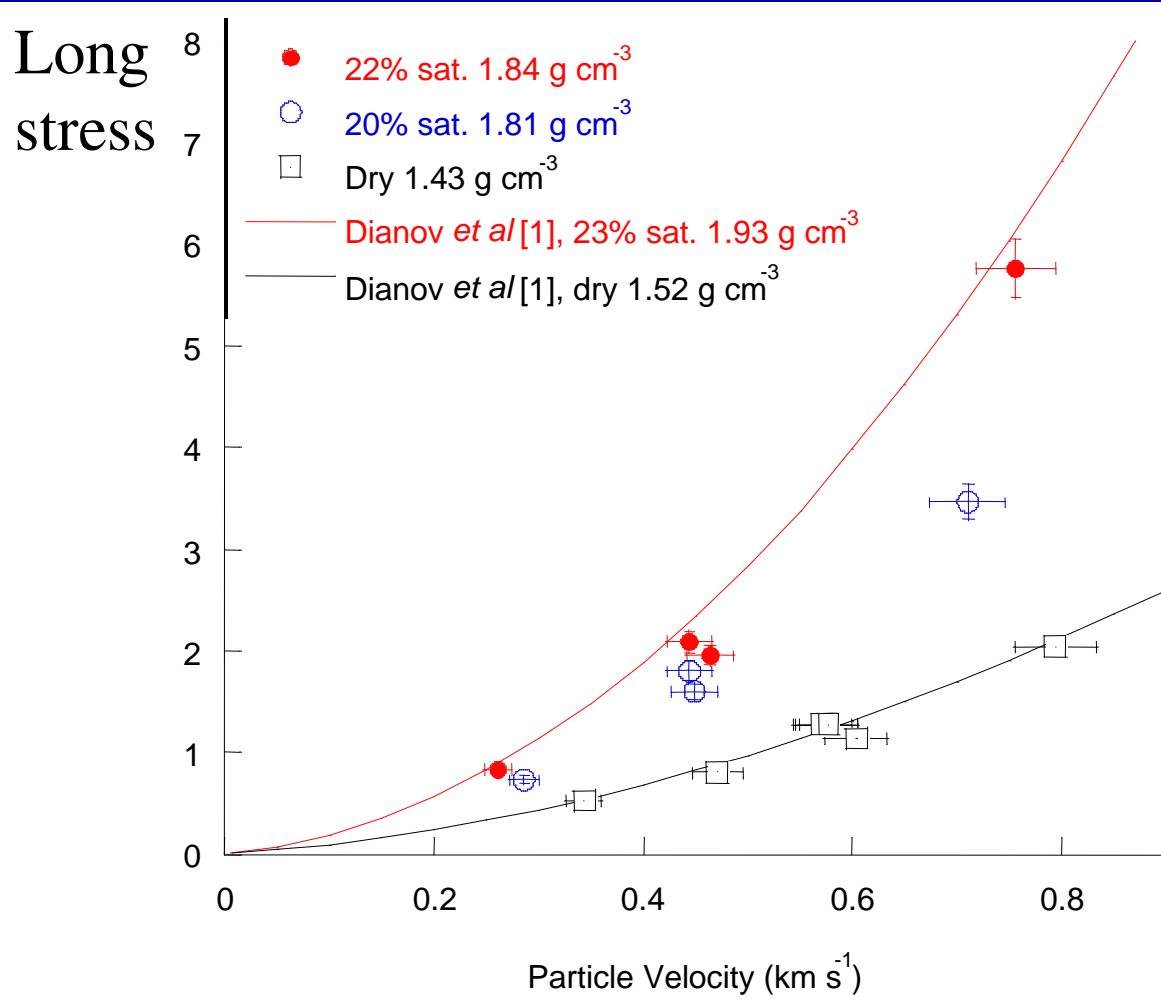
Results Combined Stress + Pressure



Water content Particle Velocity Space



Stress Space



Effect of Water Content

- 0-10% water (weight) ~ dry
- 10 - 20 % marked change
 - Higher level, faster sound speed
- Change 20 to 22% as large as from 10 - 20%

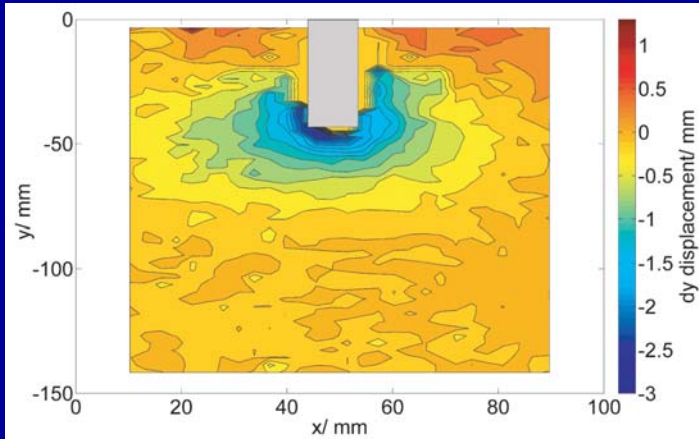
Conclusions

- Sand characterised over a range of conditions
- Low rate = friction / grain movement
- High rate = fracture
- Water content = strain rate dependant,
 - Low rate few % - big effect - lubrication
 - Intermediate rate - stronger effect at higher levels
 - High rate -small % water, no effect (>10%)
 - Large effect small % change at high saturation
- Measured Bulk Response
- Low-density sample shows different strain rate dependance, compaction processes

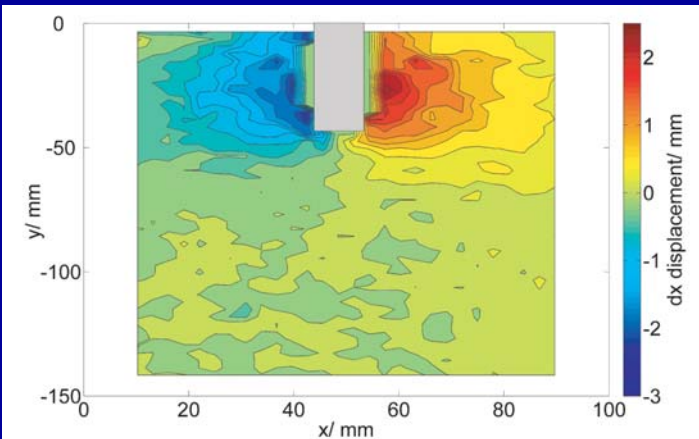
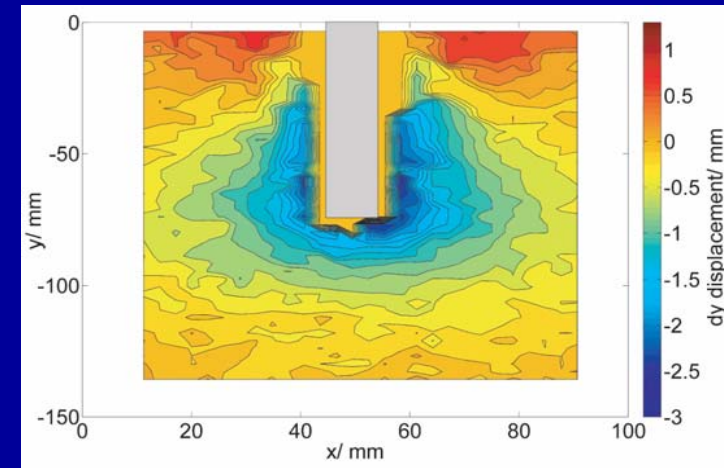
Recent / On-going Areas

- Grain size over a wider interval
- Find size / volume element that can be used to describe bulk response
- Model the fracture, collapse process
- Meso-level modelling
- Ductile grains

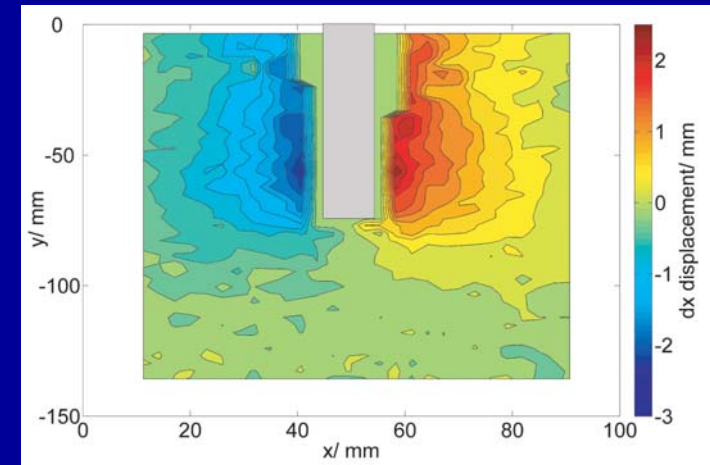
Dyanmic Impact - Longitudinal and Lateral components



1. Expanding cone shaped area of material moving longitudinally
2. Fixed angle of cone through all images



1. Lateral displacement roughly uniform along rod
2. Same lateral extent of deformation throughout



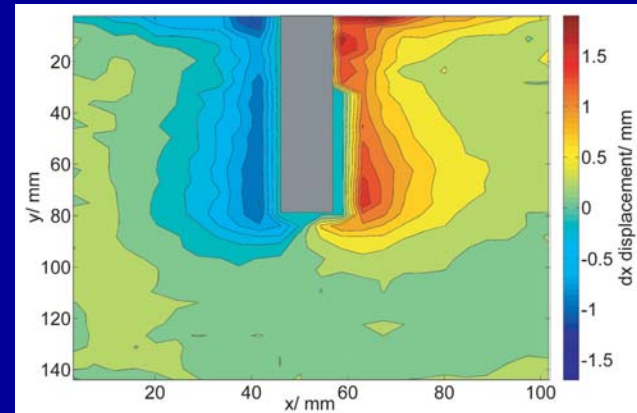
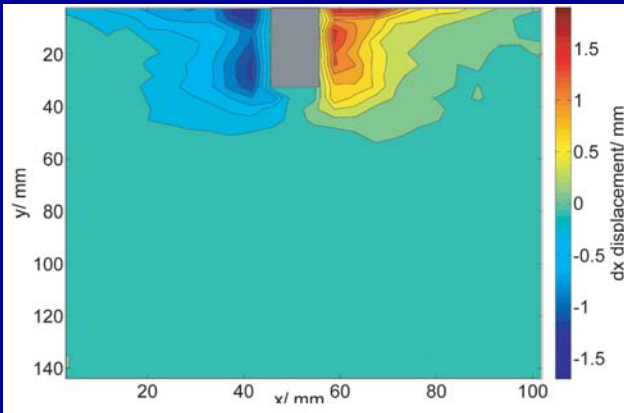
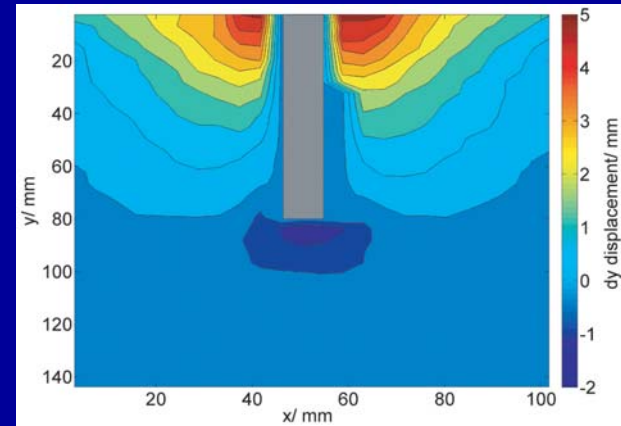
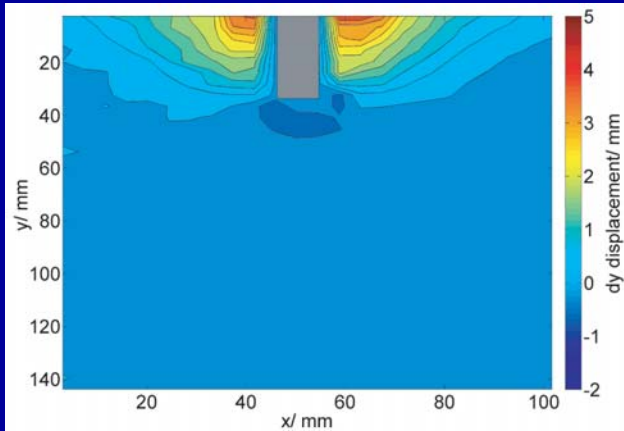
250us after impact

450us after impact

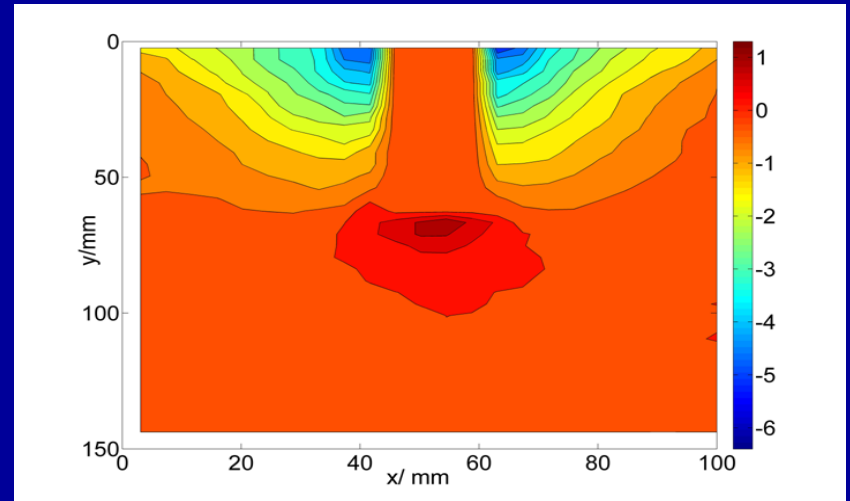
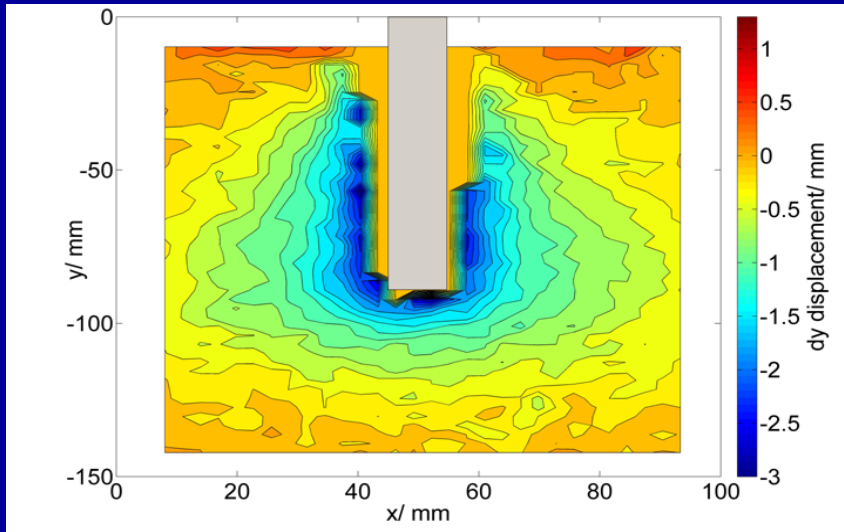
Quasi-static penetration

- Penetration carried out at a rate of 1.5 mm/min (2.5×10^{-5} m/s) using an Instron compressive tester.
- Same sample geometry, projectile, x-ray setup etc.
- Looking for rate dependence in the penetration process - will give a fuller understanding of the behaviour of the material

Longitudinal and Lateral components



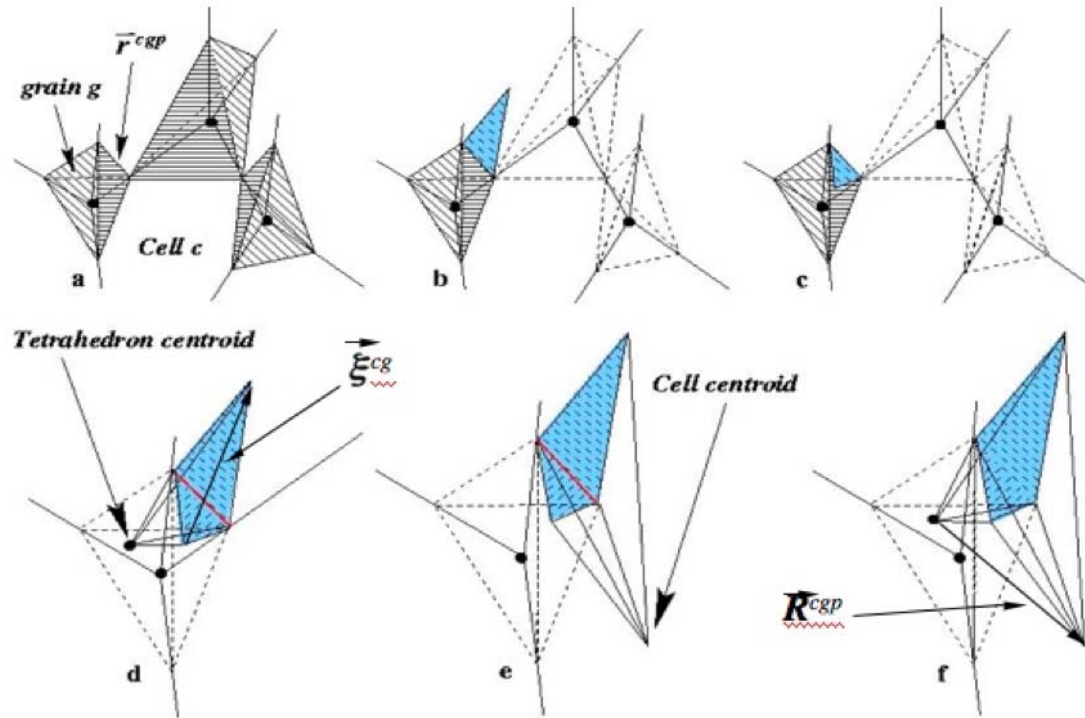
Comparison



- In the quasi-static case most of the material down to the rod tip is moving upwards
- There is no travelling compaction wave in the material

Theoretical Construct

R. Blumenfeld



$$C_{ij}^{cgp} = \left(\vec{\xi}^{cgp} \times \vec{r}^{cgp} \right)_i R_j^{cg}$$

$$V^g = V^{cgp} = \frac{1}{3} \text{Tr}\{\vec{C}^{cgp}\}$$

Acknowledgements

- D.L.A. Cross, R. Flaxman, D. Johnson, R. Marrah - Cavendish Laboratory
- D. Tam and L. Taylor - NSWC - 2002
- J. Sheridan - dstl
- Phil Church *et al.* at QinetiQ
- William Cooper, Mark Green, Kevin La Rochelle, Richard Lewis - 2006/2007
- William Weir - MoD
- Vitali Nesterenko & Marc Meyers, UCSD
- EOARD / QinetiQ / EPSRC / NSWC / Eglin AFB